# Thermal studies of Cr<sub>2</sub>O<sub>3</sub> doped CaCO<sub>3</sub>-SiO<sub>2</sub> **(2:1) system**

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Mixtures of CaCO<sub>3</sub>: SiO<sub>2</sub> in 2:1 molar ratio were subjected separated to thermal analysis with varying concentration of Cr<sub>2</sub>O<sub>3</sub> (0.1 to 5%) as dopant. The activation energy ( $E_a$ ) and enthalpy  $(\Delta H)$  shows a decreasing trend with 0.1 to 1% Cr<sub>2</sub>O<sub>3</sub> and attains a minimum value with 1% dopant. 0.1 to 0.5%  $Cr_2O_3$  helps in the formation of  $\beta$  and  $\gamma$  C<sub>2</sub>S, (Cement Chemistry notations,  $C = CaO$ ,  $S = SiO<sub>2</sub>$ ) phases at 1400°C and above but 1%  $Cr<sub>2</sub>O<sub>3</sub>$  stabilizes  $\beta$ -C<sub>2</sub>S phase along with a little free lime and CaCrO<sub>4</sub>. A small quantity of CaCrO<sub>4</sub>, Cr<sub>2</sub>SiO<sub>4</sub> and  $\alpha$ -C<sub>2</sub>S are also formed along with the major phases with 5%  $Cr_2O_3$  indicating that  $Cr^{3+}$  can substitute both Ca<sup>2+</sup> and Si<sup>4+</sup> ions in the C<sub>2</sub>S lattice.

# 1. **Introduction**

The effect of minor constituents on the structural properties of portland cement clinker has been the subject of interest for many years  $[1-6]$ . The effects of  $Cr_2O_3$  on the early strength development have been reported [7-9]. Investigations on the effect of  $Cr_2O_3$ on the formation of di- and tri-calcium silicate phases have also been carried out [10-13]. However, little work has been done on the thermal behaviour of  $Cr_2O_3$ doped mixture of 2:1 molar  $CaCO<sub>3</sub>$ : SiO<sub>2</sub>, although the above mix is relevant for the synthesis of dicalcium silicate, an important mineral constituent of clinker.

This work aims to evaluate the thermodynamic and kinetic parameters of the decomposition of  $CaCO<sub>3</sub>$  in  $Cr_2O_3$  doped 2:1 molar  $CaCO_3-SiO_2$  mixture and on the early formation of dicalcium silicate phase. From the industrial point of view, the study is also important since the chromium acts as a mineralizer in the early formation of cement constituents [10, 13] and accelerates the assimilation of CaO and  $SiO<sub>2</sub>$ .

### **2. Experimental details**

#### 2.1. Materials and sample **preparation**

To the 2 : 1 molar mixture of reagent grade  $CaCO<sub>3</sub>$  and quartz powder (purity  $> 99.9\%$ ), varying amounts of  $Cr_2O_3$  (0.1 to 5%) were added. The resulting mixtures after thorough mixing, grinding and passing through a  $100 \mu m$  sieve, were shaped in the form of nodules with small amounts of distilled water. The samples after drying at 100  $\pm$  5° C (2 h) were tested for quantitative estimation of  $CaCO<sub>3</sub>$  to ensure complete homogenization. These dried samples were stored for the experimental work.

### 2.2. Thermal analysis

The measurements were made by Mettler thermal analyser  $(TA-1)$ , which simultaneously records the differential thermal analysis (DTA) differential thermal gravimetric (DTG) and thermal gravimetric (TG) curves. The samples (60 mg) were heated to  $1450^{\circ}$  C at a rate of  $8^{\circ}$ Cmin<sup>-1</sup> in a platinum crucible of the thermal analyser.  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> (previously burned to  $1500^{\circ}$  C for 30 min) was used as the reference material.

The activation energy  $(E_a)$  of CaCO<sub>3</sub> decomposition was calculated from the DTG curve [14]. The enthalpy  $(\Delta H)$  and the shape index were determined from the DTA curve [15, 16].

### **2.3. X-ray diffraction** studies

The samples for analysis were powdered to pass through a  $45 \mu m$  sieve and pressed into a sample holder. The instrument used was Philips model PW 1120. The diffraction patterns were recorded using copper target and nickel filter.

### 2.4. **Examination of the intermediate** phases

The samples in the form of nodules were heated in a quench furnace at the rate of  $8^{\circ}$  C min<sup>-1</sup> in a platinum bucket to the temperature where the DTA peak ends, retained for 30 min at that temperature and immediately quenched in liquid nitrogen. Thus the likelihood of the reversibility of the reaction was prevented.

### **2.5. Estimation of free lime**

The free lime in the final products (obtained after heating to the final DTA peak temperature for 2h) was estimated by titrating the ethylene glycol extract against standard HCI [17].

## **3. Results and discussion**

A broad exotherm in the DTA curve was observed for all samples in the region 100 to  $200^{\circ}$  C (Fig. 1), which could be assigned to heat capacity changes since no features are observed in the DTG curve. An endothermic peak at 575° C due to  $\alpha-\beta$  quartz transformation is not influenced by the presence or concentration of the dopant. The initial, peak and termination temperatures  $(T_i, T_d$  and  $T_f$  respectively) of the DTG peak

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*Figure 1* Thermal curves of (a)  $2CaCO<sub>3</sub>$ : SiO<sub>2</sub>; (b)  $2CaCO_3:SiO_2 + 0.1\%$  Cr<sub>2</sub>O<sub>3</sub>; (c)  $2CaCO_3:SiO_2 + 0.5\%$  Cr<sub>2</sub>O<sub>3</sub>; (d)  $2CaCO<sub>3</sub>$ : SiO<sub>2</sub> + 1% Cr<sub>2</sub>O<sub>3</sub>; (e)  $2CaCO<sub>3</sub>$ :  $SiO_2 + 5\%$   $Cr_2O_3$  (---) DTG curve,  $\left(\begin{matrix}-\end{matrix}\right)$  DTA curve.

for decomposition of  $CaCO<sub>3</sub>$  and the activation energy  $(E_a)$  are given in Table I. The enthalpy  $(\Delta H)$ and shape index (Fig. 2) determined from the DTA curves are also given in the table. The dopant reduces the values of  $T_i$ ,  $T_d$  and  $T_f$  but the effect of concentration variation is not significant. As the amount of dopant increases from 0.1 to 1.0%, the  $E_a$  and  $\Delta H$ values progressively decrease, but for 5% concentration these values show an increase. The shape index shows an increasing trend with increasing concentration of the dopant and the value of the reaction kinetics approaches one.

The thermal curves of these samples show an exotherm at  $1210^{\circ}$ C, which could be attributed to the transformation of quartz into cristobalite and formation of some  $\beta$  and  $\gamma$ -C<sub>2</sub>S phases. This is confirmed by the X-ray diffraction (XRD) pattern of the liquid nitrogen quenched sample heated to  $1220^{\circ}$ C (with 30 min retention).

0.1% doped  $Cr_2O_3$  sample gives an exothermic peak

TABLE I\* Thermal analysis data of  $Cr_2O_3$  doped  $CaCO_3$ : SiO<sub>2</sub> (2:1) system

Concentration of $Cr_2O_3$ by weight in $CaCO_3:SiO_2$ $(2:1)$ system	Temperature of decomposition of CaCO <sub>3</sub> and other kinetic parameters						Exothermic peak
	Threshold $(T_i)$ (°C)	Peak $(T_{\rm d})$ (°C)	Termination $(T_f)$ (°C)	Activation energy $E_{\rm a}$ (kJ mol <sup>-1</sup> )	Enthalpy $\Delta H$ (kJ mol <sup>-1</sup> )	Shape index from DTA	observed by DTA after decomposition of $CaCO3 (^{\circ}C)$
0.0	740	885	910	247	160	0.143	1425
0.1	655	860	885	225	146	0.250	1420 1440
0.5	680	860	900	216	142	0.307	1410
1.0	680	860	890	202	139	0.360	1400 1420
5.0	700	870	890	210	156	0.419	1420

\*An endotherm at  $575^{\circ}$ C and an exotherm at  $1210^{\circ}$ C comon to all curves are not given in the table.



*Figure 2* Shape index of the decomposition peak (DTA).

at both  $1420$  and  $1440^{\circ}$  C. The sample heated to  $1430^{\circ}$  C (30 min retention) and quenched in liquid nitrogen shows the presence of  $\beta$  and  $\gamma$ -C<sub>2</sub>S phases with high free lime as discerned by XRD. The same mix on heating to  $1450^{\circ}$  C (30 min retention) gives mostly  $\gamma$ -C<sub>2</sub>S and small amounts of  $\beta$ -C<sub>2</sub>S phases. The mix on firing for 1 h at  $1450^{\circ}$  C gives the same pattern with a constant value of free lime  $(0.8\%)$ .

0.5%  $Cr_2O_3$  gives an exothermic peak at 1410°C. The sample heated to  $1420^{\circ}$ C and quenched in liquid nitrogen gives again a mixture of  $\beta$  and  $\gamma$ -C<sub>2</sub>S phases with an increase in  $\beta$ -C<sub>2</sub>S phase. Longer heating of the sample at this temperature does not change the XRD pattern or the free lime content (0.6%).  $1\%$  Cr<sub>2</sub>O<sub>3</sub> gives two exotherms at 1400 and  $1420^{\circ}$  C and the liquid nitrogen quenched sample heated at  $1410^{\circ}$  C (30 min retention) gives  $\beta$ -C<sub>2</sub>S phase along with small amounts of free lime (0.5%) and  $Cr_2SiO_4$ . This is inferred from the increase in the intensities of peak for free lime at  $d$ nm0.24. This position is also reported for Cr<sub>2</sub>SiO<sub>4</sub> along with other  $d$  values (0.27, 0.16 and 0.20 nm).

 $\gamma$ -C<sub>2</sub>S phase is not observed. This is in accordance with the study done by Pashchenko *et al.* [18]. DTA of 5%  $Cr_2O_3$  doped sample gives an exotherm at 1420° C. XRD pattern of the liquid nitrogen quenched sample gives the most predominant  $\beta$ -C<sub>2</sub>S phase along with small quantity of  $\alpha'$ -C<sub>2</sub>S phase. Some of CaCrO<sub>4</sub> and  $Cr_2SiO_4$  are also formed as discerned from the lines of the XRD pattern. Free lime content remains the same (0.5%). The final products so formed are given in Table II. The XRD pattern of the phases formed at the final DTA peak temperature are shown in Fig. 3.

Fig. 4 shows the ratio of phases  $(\gamma$ -C<sub>2</sub>S/ $\beta$ -C<sub>2</sub>S) formed at  $1450^\circ$  C by addition of the different percentage of  $Cr_2O_3$  dopant (XRD line intensity ratio has been used). It is clear from the figure that ratio of  $\gamma$  to  $\beta$  dicalcium silicate phase decreases with increasing percentage of chromium oxide.

#### **4. Conclusion**

Smaller concentration of  $Cr_2O_3$  (0.1%) favours the formation of  $\gamma$ -C<sub>2</sub>S phase. Higher percentages (0.5 to 5%) lead to the formation of the more desired  $\beta$ -C<sub>2</sub>S phase.  $1\%$  Cr<sub>2</sub>O<sub>3</sub> is found to be most effective in the decomposition of  $CaCO<sub>3</sub>$  (minimum activation energy) and formation of  $\beta$ -C<sub>2</sub>S with complete elimination of  $\gamma$ -C<sub>2</sub>S phase. 5% Cr<sub>2</sub>O<sub>3</sub> gives most predominantly  $\beta$ -C<sub>2</sub>S phase along with some  $\alpha'$ -C<sub>2</sub>S, CaCrO<sub>4</sub> and  $Cr_2SiO_4$ . This implies that  $Cr^{3+}$  causes a hole defect by replacing Ca<sup>2+</sup> and Si<sup>4+</sup> ions from the C<sub>2</sub>S lattice. The temperature of  $\beta$ -C<sub>2</sub>S formation is not affected by any concentration of  $Cr_2O_3$ .

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*Figure 3* X-ray diffraction of chromium doped dicalcium silicate phase:  $A =$  $\gamma$ -C<sub>2</sub>S; B =  $\beta$ -C<sub>2</sub>S; C = free lime;  $D = CaCrO<sub>4</sub>; E = Cr<sub>2</sub>SiO<sub>4</sub>; F = \alpha'$  $C_2S$ .

TABLE II Products formed at the various exothermic peaks (observed by DTA) of thermal curves as discerned by X-ray diffraction



\* ASTM X-ray Powder Diffraction Files.

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*Figure 4* Ratio of  $\gamma$ -C<sub>2</sub>S/ $\beta$ -C<sub>2</sub>S against concentration of dopant.

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